

CHAPTER 37

Performance Evaluation of Paver Blocks Made with Recycled Concrete Aggregate (RCA) and Recycled Concrete Fine Aggregate (RCFA)

Meraz Ali, Gauresh Shetty**, Devesh Nauhawar** and Rihan Maaze****

ABSTRACT

The construction sector consumes a vast number of natural aggregates and generates a large volume of construction and demolition (C&D) waste, leading to environmental degradation and resource depletion. Much of this waste is improperly managed, causing unsustainable disposal practices. This study investigates the sustainable production of paver blocks (as per IS 15658:2021 – Precast Concrete Blocks for Paving – Specification) by partially replacing natural aggregates with recycled concrete aggregates (RCA) and recycled fine aggregates (RFA) derived from C&D waste. The experimental program uses a Taguchi L9 orthogonal array design to optimize mix proportions and evaluate the effects of RCA and RFA replacement levels on the mechanical performance of paver blocks. The recycled aggregate-based paver blocks were tested and compared with conventional cement concrete paver blocks to determine an optimal mix that ensures structural integrity and sustainability. This research addresses a crucial issue in sustainable construction, promoting a circular economy by reusing waste materials and reducing dependence on virgin resources. The results are expected to demonstrate that incorporating RCA and RFA in paver block production not only minimizes environmental impact but also offers a cost-effective and eco-friendly alternative for modern construction practices.

Keywords: RCA , RCFA , Paver Block, Performance.

1.0 Introduction

Major consumer of natural aggregates, the construction industry is also a very great source of construction and demolition (C&D) waste.

**Corresponding author; Student, School of Construction, NICMAR University, Pune, Maharashtra, India (E-mail: p24700564@student.nicmar.ac.in)*

***Student, School of Construction, NICMAR University, Pune, Maharashtra, India (E-mail: p24700588@student.nicmar.ac.in; p24700583@student.nicmar.ac.in)*

****School of Engineering, NICMAR University, Pune, Maharashtra, India (E-mail: rihanmaaz@gmail.com)*

The high rate of urbanization in India has contributed to more rapid loss of natural resources, and more burdening landfills as a result of improper disposal of C&D waste. Recycled Concrete Aggregate (RCA) or Recycled Concrete Fine Aggregate (RCFA) that are the by-products of the demolished concrete also provide a viable substitute to the conventional fine aggregates in concrete products like paver blocks (Bayram & Greiff, 2023).

Paver blocks consist of concrete that is common in pavements, parking space, footways, and roads that are less busy. Their workability, compressive strength, density, and the properties of durability like water absorption are the main factors of their performance. The current research uses a Taguchi L9 orthogonal array (3 factors x 3 levels) to maximize mix ratios and determine the impact of RCA and RCFA substitution on the performance of paver blocks.

2.0 Significance and Objectives of the Research

2.1 Research significance

Recycling of RCA and RCFA helps to sustain the construction through eliminating the need to use virgin aggregates, decreasing the environmental impact, and fostering the ideas of the circular economy (Merecycled et al., 2012). Nevertheless, the uncertainty of the recycled aggregate properties is such that it requires experimental validation on a large scale, which should be controlled.

2.2 Objectives

The main objectives of this study are as follows:

1. To utilize Recycled Concrete Aggregate (RCA) and Recycled Concrete Fine Aggregate (RCFA) in the production of paver blocks.
2. To evaluate the compressive strength of paver blocks containing recycled aggregates.
3. To study the flexural strength of paver blocks produced with recycled aggregates.
4. To analyse the water absorption characteristics of the paver blocks.
5. To compare the performance of recycled aggregate paver blocks with conventional paver blocks.
6. To assess the feasibility of using RCA and RCFA for sustainable construction applications.

3.0 Materials and Experiment Process

3.1 Materials

1. Ordinary Portland cement (OPC).
2. Natural Coarse Aggregate (control)

3. Recycled Concrete Aggregate (RCA).
4. Recycled Concrete Fine Aggregate (RCFA).
5. Potable water

The material properties were established according to the IS 2386 and the IS 4031 standards.

3.2 Experimental design

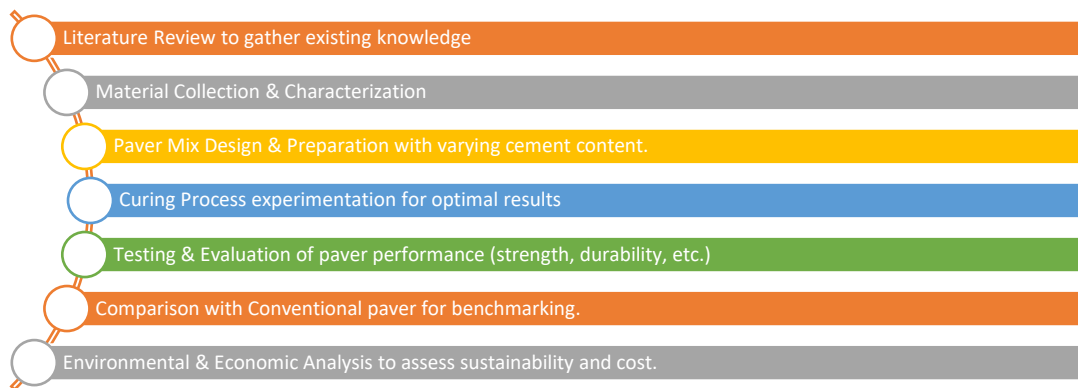
An orthogonal array of Taguchi L9 was accepted with three factors with three levels:

- RCA replacement (%)
- RCFA replacement (%)
- Cement content (fixed- mix independent)

This will reduce the number of experiments and yield statistical strength.

3.3 Research methodology

Figure 1: Flow Chart of Research Methodology



Source: Created by authors

3.4 Testing program

The following were the tests:

The water absorption and specific gravity of RCA and RCFA.

- Slump cone test
- Compaction factor test
- Density Fresh and hardened Fresh.
- Paved block uptake of water.
- Compressive strength test (28 day)
- Split tensile strength and Flexural Strength
- Abrasion Value

All the tests were conducted according to the IS 15658: 2006 and IS 516.

4.0 Discussion and Results of the Experiments

A workability characteristic is a property that is sought after but remains unstated. Workability is an attribute that is desired but not defined. The results of slump and compaction factor suggest that the workability decreases gradually with an increase in content of RCA and RCFA because of the enhancement of the water absorption of recycled aggregates and roughness of their surfaces, as was observed previously (Kadam et al., 2024).

4.1 Density characteristics

The fresh and hardened density values demonstrated a slight decrease with increase in the recycled content of aggregate, and it is because of the low specific gravity and porous structure of RCA and RCFA.(Tawalare et al., 2018)

The water absorption of paver blocks was studied, and the results are presented below. Water uptake rose as RCFA content rose because of finer particles and increased porosity. But still, the values were within the acceptable range in the case of non-structural and medium-traffic applications with pavers.

4.2 Strength performance- compressive

The outcomes of compressive strength will be added to the dataset when they are available. According to the literature, moderation levels of replacement will be sufficient to satisfy the requirements of the IS 15658 of paver blocks in pedestrian and light-traffic areas (Tawalare et al., 2018)

5.0 Experimental Data Table

Table 1: Summary of Experimental Results for Taguchi L9 Mixes

Mix ID	RCA (%)	RCFA (%)	Compressive Strength (MPa)
M1	0	0	33.245
M2	50	50	32.193
M3	50	75	31.164
M4	50	100	30.135
M5	75	50	30.576
M6	75	75	29.547
M7	75	100	28.518
M8	100	50	29.253
M9	100	75	28.224
M10	100	100	27.195

Source: Created by authors

Table 2: Water Absorption Test Results

Material	Weight Before Oven Dry (g)	Weight After Oven Dry (g)	Difference (g)	Formula Used	Water Absorption (%)
RFA (Recycled Fine Aggregate)	2010	1803.5	206.5	$\frac{SSD - OD}{OD} \times 100$	11.45 %
RCA (Recycled Coarse Aggregate)	2020	1978	42	$\frac{SSD - OD}{OD} \times 100$	2.12 %

Source: Created by authors

Table 3: Specific Gravity Test (Recycled Fine Aggregate)

Parameter	Description	Value (g)
W1	Weight of empty pycnometer	638.9
W2	Weight of pycnometer + dry aggregate	1140.8
W3	Weight of pycnometer + aggregate + water	1803.9
W4	Weight of pycnometer + water	1511.7
Specific Gravity (SG_FA)	Calculated value	2.393

Source: Created by authors

Table 4: Specific Gravity Test (Recycled Coarse Aggregate)

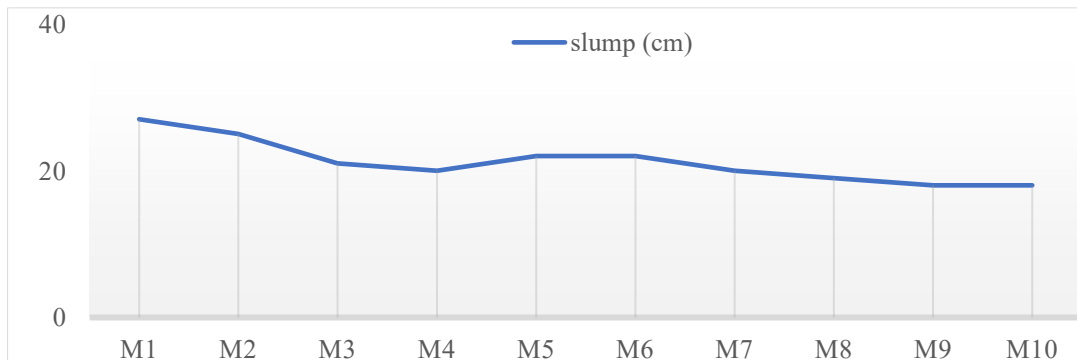
Parameter	Description	Value (g)
W1	Weight of empty pycnometer	633.8
W2	Weight of pycnometer + dry aggregate	1134.3
W3	Weight of pycnometer + aggregate + water	1822.8
W4	Weight of pycnometer + water	1504.8
Specific Gravity (SG_CA)	Calculated value	2.742

Source: Created by authors

4.0 Experimental Results and Discussion

4.1 Workability characteristics

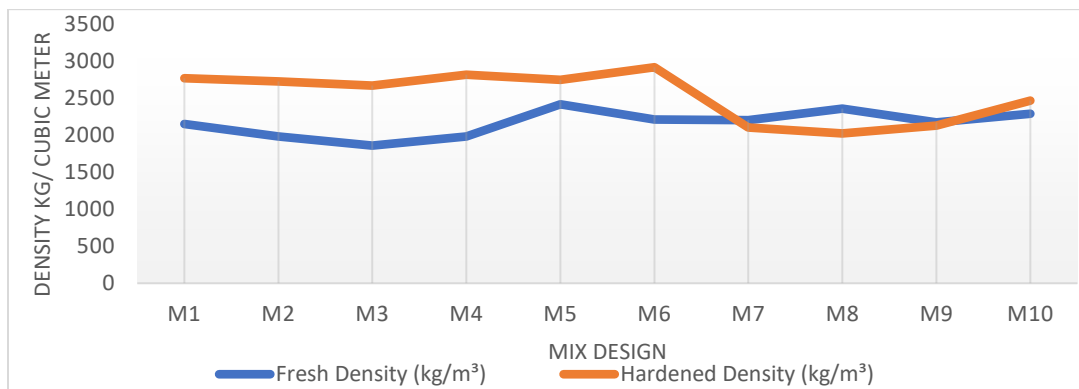
Slump cone and compaction factor tests were used to determine the workability of fresh concrete mixes, and the findings revealed a steady decrease in the proportion of fresh concrete mixes with increasing proportions of RCA and RCFA. This decrease is due to the increased water uptake capacity and rough and sharp surface texture of the recycled aggregates due to the presence of old mortar. With a smaller particle size and larger porosity, RCA exhibited a stronger effect on loss of workability than RCA. The same tendencies were also mentioned in the recent literature, with higher levels of recycled aggregates leading to higher water requirements and decreased plasticity of concrete blends (Bayram & Greiff, 2023).

Figure 2: Workability vs Mix ID

Source: Created by authors

4.2 Density characteristics

Fresh and hardened density values of the paver blocks showed a slight declining tendency with level of replacement of RCA and RCFA. This tendency is mainly because the specific gravity of recycled aggregates and their porous microstructure are lower compared to those of natural aggregates. Adhered mortar and internal microcracks are also present in RCA that leads to a lower unit weight that has also been noted in other experimental studies of recycled aggregate paver blocks (Shrivastava & Chini, 2009).

Figure 3: Density vs Mix ID

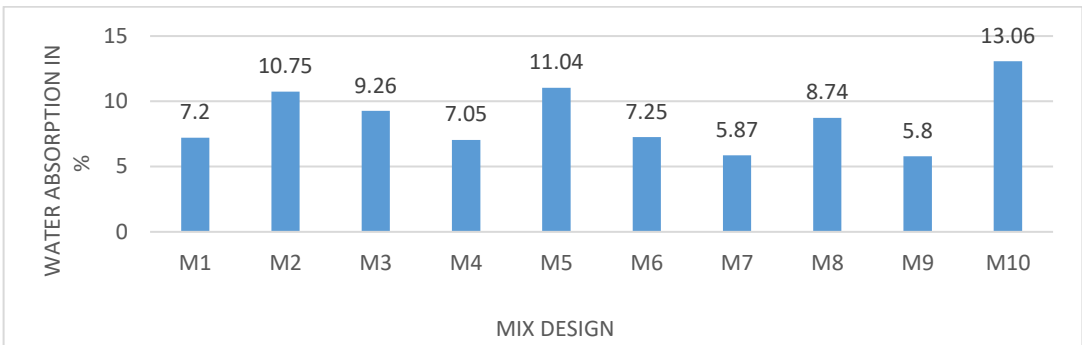
Source: Created by authors

4.3 Paver blocks absorption of water

The absorption of hardened paver blocks by water was also greater when the content of RCFA was increased because recycled fine aggregates contained finer particles and had

greater porosity. However, the obtained values did not exceed the allowable levels given in non-structural and medium-traffic paver utilization, which is consistent with the recent results on RCA-RCFA-based paver blocks (Tawalare et al., 2018)

Figure 4: Water Absorption vs Mix ID

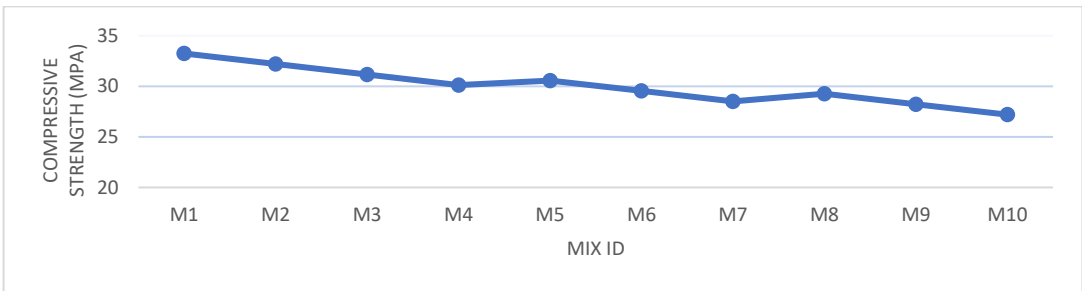


Source: Created by authors

4.4 Compressive strength performance

The findings of compressive strength show a gradual decrease of compressive strength with the level of RCA and RCFA replacement.

Figure 5: Compressive Strength vs Mix ID



Source: Created by authors

Nevertheless, mixes with medium replacement levels (up to about 50 percent) showed strengths that could be used in pedestrian and light-traffic applications, meeting the standards of IS 15658. The observation aligns with the modern research and reports that recycled aggregate content optimized by incorporating sufficient mechanical performance and increasing sustainability (Bayram & Greiff, 2023).

Purpose: Shows overall strength variation across Taguchi L9 mixes.

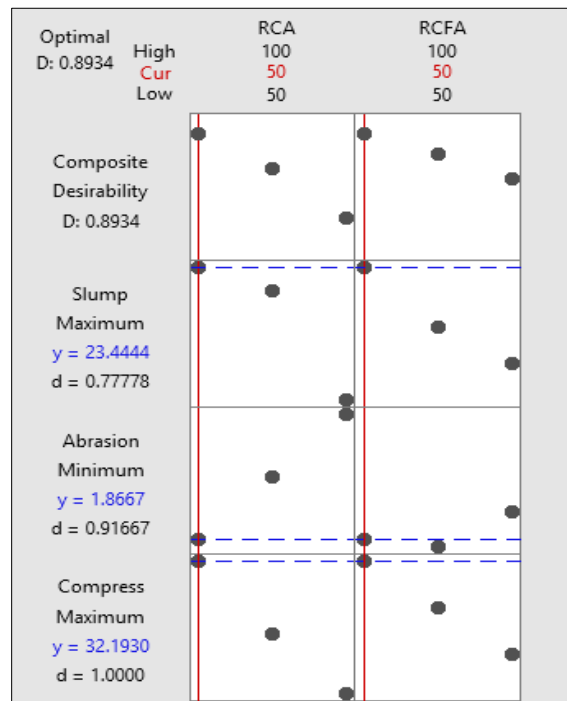
5.0 Master Experimental Data Table

Table 5: Summary of Experimental Results for Taguchi L9 Mixes

Mix	Cement	Virgin Aggregate		Recycled Aggregates		Water	Fresh Density (kg/m ³)	Hardened Density (kg/m ³)	Compressive Strength (MPa)	Split Tensile Strength (MPa)	Flexural Strength (MPa)	Abrasion Value (mm)	Water Absorption (%)	Slump (mm)
		Fine Aggregate	Coarse Aggregate	RCFA	RCA									
M1	100	100	100	0	0	40	2150	2764	33.245	3.32	4.65	1.6	7.2	27
M2	100	50	50	50	50	40	1979	2723	32.193	3.21	4.5	1.8	10.75	25
M3	100	50	25	50	75	40	1857	2667	31.164	3.1	4.36	1.9	9.26	21
M4	100	50	0	50	100	40	1979	2814	30.135	3	4.22	2	7.05	20
M5	100	25	50	75	50	40	2414	2743	30.576	3.05	4.28	2.2	11.04	22
M6	100	25	25	75	75	40	2207	2914	29.547	2.95	4.14	2.1	7.25	22
M7	100	25	0	75	100	40	2200	2100	28.518	2.85	3.99	2.3	5.87	20
M8	100	0	50	100	50	40	2357	2021	29.253	2.92	4.09	2.5	8.74	19
M9	100	0	25	100	75	40	2171	2129	28.224	2.82	3.95	2.4	5.8	18
M10	100	0	0	100	100	40	2287	2465	27.195	2.72	3.81	2.6	13.06	18

Source: Created by authors

Figure 6: Multi-Response Optimization Plot (Taguchi Response Optimizer)



Source: Created by authors

6.0 ANOVA Analysis

Table 6: ANOVA Summary

Response	Recycled Concrete Aggregate P-value	Recycled Concrete Fine Aggregate P-value	R ²
Compressive Strength	*	*	100%
Abrasion	0.001	0.049	97.78%
Slump	0.048	0.138	83.98%

Source: Created by authors

The ANOVA results indicate that Recycled Concrete Aggregate is statistically significant for abrasion and slump because its P-values are below 0.05. For abrasion, Recycled Concrete Aggregate shows very high significance (0.001), while Recycled Concrete Fine Aggregate, is also significant (0.049). For slump, Recycled Concrete Aggregate is significant whereas Recycled Concrete Fine Aggregate, is less significant. The high R² values confirm that the regression model explains most of the response variation, indicating strong reliability of the optimization model.

Table 7: parameter of 3 tests

Response	Goal	Lower	Target	Upper	Weight	Importance
Slump	Maximum	18.000	25.000		1	1
Abrasion Value	Minimum		1.800	2.6	1	1
Compressive Strength	Maximum	27.195	32.193		1	1

Source: Created by authors

Table 8: Final Optimized Mix

Recycled Concrete Aggregate	Recycled Concrete Fine Aggregate	Slump	Abrasion	Compressive Strength	Desirability
50	50	23.444	1.867	32.193	0.893

Source: Created by authors

The multi-response optimization selected 50% Recycled Concrete Aggregate and 50% Recycled Concrete Fine Aggregate, as the optimum mix because it simultaneously produced the highest compressive strength, acceptable abrasion resistance, and suitable workability. The desirability value of 0.893 indicates that the selected mix is very close to ideal optimization. This confirms that moderate recycled aggregate replacement provides the best balance between sustainability and engineering performance for M30 grade paver blocks.

7.0 Conclusions

The current research will ascertain that Recycled Concrete Aggregate (RCA) and Recycled Concrete Fine Aggregate (RCFA) can be successfully used in the manufacturing of concrete paver blocks on a controlled basis when used in the specific proportions that will aid in the sustainable construction (Tawalare et al., 2018). The findings show that increment in the contents of RCA and RCFA results in slight decrease in workability, density and compressive strength because of the increased porosity and water absorption, but mixes with intermediate replacement rates (up to 50 percent) gave performances suitable in pedestrian and light-traffic applications. Taguchi L9 orthogonal array was also an efficient optimization tool that allowed to do systematic analysis of multiple variables with less effort during experiments. These results coincide with the latest research on the viability of the recycled aggregates in the concrete products and encourage the principles of the circular economy and preservation of the resources (Kadam et al., 2024).

References

1. Poon, C.S., & Chan, D. (2006). Paving blocks made with recycled concrete aggregate and crushed clay brick. *Construction and Building Materials*, 20(8), 569–577.
2. Kumar, G., Shrivastava, S., & Gupta, R.C. (2020). Impact of recycled concrete aggregate on mechanical and durability properties of concrete paver blocks. *Materials Today: Proceedings*, 27, 780–785.
3. Attri, G.K., Gupta, R.C., & Shrivastava, S. (2021). Impact of recycled concrete aggregate on mechanical and durability properties of concrete paver blocks. *Materials Today: Proceedings*, 43, 780–785.
4. Sivamani, J. (2023). Performance studies on energy efficient paver block with treated recycled aggregate. *Research on Engineering Structures and Materials*, 9(3), 541–550.
5. Robayo-Salazar, R., Valencia-Saavedra, W., & Mejía de Gutiérrez, R. (2022). Reuse of powders and recycled aggregates from mixed construction and demolition waste in alkali-activated materials and precast concrete units. *Sustainability*, 14(14), 9685.
6. Pederneiras, C.M., Durante, M.D.P., Amorim, E.F., & Ferreira, R.L. (2020). Incorporation of recycled aggregates from construction and demolition waste in paver blocks. *Revista IBRACON de Estruturas e Materiais*, 13, e13405.
7. Kadam, P.P., Maske, M.M., & Patil, S.N. (2024). Development of eco-friendly paving blocks using waste plastic and construction demolition waste. *AIP Conference Proceedings*.

8. Bayram, B., & Greiff, K. (2023). Life cycle assessment on construction and demolition waste recycling: A systematic review analyzing three important quality aspects. *The International Journal of Life Cycle Assessment*, 28(8), 967-989.
9. MeRecycled Concrete Aggregatente, I.T., Bovea, M.D., Ibáñez-Forés, V., & Arena, A.P. (2012). Life cycle assessment of construction and demolition waste management systems: A Spanish case study. *The International Journal of Life Cycle Assessment*, 17, 232-241.
10. Touran, A., Christoforou, C., Dantata, N., & Wang, J. (2004). An estimating system for construction and demolition waste management. *Journal of Solid Waste Technology and Management*, 30(2), 81-89.
11. Shrivastava, S., & Chini, A. (2009). Construction materials and C&D waste in India. *Lifecycle Design of Buildings, Systems and Materials*.
12. Ganjian, E., Jalull, G., & Sadeghi-Pouya, H. (2015). Using waste materials and by-products to produce concrete paving blocks. *Construction and Building Materials*, 77, 270-275.
13. Tawalare, A., Kejkar, R., & Kumar, M. (2018). Comparison of geopolymer paver block using natural aggregate and recycled aggregate as fine aggregate and slag as coarse aggregate. *IOP Conference Series: Materials Science and Engineering*.
14. Fanijo, E.O. (2023). Review on recycled aggregates in pavement construction and sustainable concrete materials. *Journal of Sustainable Construction Materials*.
15. Maraseni, S. (2025). Comparative study of eco-friendly paving blocks incorporating recycled aggregates for sustainable pavement construction. *Journal of Cleaner Production*.
16. Tam, V.W.Y., Gao, X.F., & Tam, C.M. (2005). Microstructural analysis of recycled aggregate concrete produced from two-stage mixing approach. *Cement and Concrete Research*, 35, 1195-1203.
17. Tabsh, S.W., & Abdelfatah, A.S. (2009). Influence of recycled concrete aggregates on strength properties of concrete. *Construction and Building Materials*, 23, 1163-1167.
18. Rahal, K. (2007). Mechanical properties of concrete with recycled coarse aggregate. *Building and Environment*, 42, 407-415.
19. Evangelista, L., & de Brito, J. (2007). Mechanical behaviour of concrete made with fine recycled concrete aggregates. *Cement and Concrete Composites*, 29, 397-401.
20. Kou, S.C., & Poon, C.S. (2012). Enhancing durability properties of concrete prepared with coarse recycled aggregate. *Construction and Building Materials*, 35, 69-76.
21. Silva, R.V., de Brito, J., & Dhir, R.K. (2014). Properties and composition of recycled aggregates from construction and demolition waste suitable for concrete production. *Materials and Structures*, 47, 621-634.

22. Pedro, D., de Brito, J., & Evangelista, L. (2017). Influence of the use of recycled concrete aggregates from different sources on structural concrete. *Construction and Building Materials*, 152, 734-742.
23. Bravo, M., de Brito, J., Pontes, J., & Evangelista, L. (2015). Durability performance of concrete with recycled aggregates from construction and demolition waste plants. *Construction and Building Materials*, 82, 141-151.
24. Zega, C.J., & Di Maio, A.A. (2011). Recycled concrete made with different natural coarse aggregates exposed to high temperature. *Construction and Building Materials*, 25, 2047-2052.
25. Kisku, N., Joshi, H., Ansari, M., Panda, S., Nayak, S., & Dutta, S.C. (2017). A critical review and assessment for usage of recycled aggregate as sustainable construction material. *Construction and Building Materials*, 131, 721-740.
26. Behera, M., Bhattacharyya, S.K., Minocha, A.K., Deoliya, R., & Maiti, S. (2014). Recycled aggregate from C&D waste and its use in concrete – A review. *Resources, Conservation and Recycling*, 82, 52-62.
27. Thomas, C., Setién, J., Polanco, J.A., Alaejos, P., & Sánchez de Juan, M. (2013). Durability of recycled aggregate concrete. *Construction and Building Materials*, 40, 1054-1065.
28. Ajdukiewicz, A., & Kliszczewicz, A. (2002). Influence of recycled aggregates on mechanical properties of concrete. *Cement and Concrete Composites*, 24, 269-279.
29. Akbarnezhad, A., Ong, K.C., Zhang, M.H., Tam, C.T., & Foo, T.W. (2011). Microwave-assisted beneficiation of recycled concrete aggregates. *Construction and Building Materials*, 25, 3469-3479.
30. Leite, M.B., & Monteiro, P.J.M. (2016). Durability of recycled aggregate concrete: A review. *Waste Management*, 45, 101-115.
31. Malešev, M., Radonjanin, V., & Marinković, S. (2010). Recycled concrete as aggregate for structural concrete production. *Sustainability*, 2, 1204-1225.
32. González-Fonteboa, B., & Martínez-Abella, F. (2008). Concrete with aggregates from demolition waste and silica fume. *Materials and Mechanical Properties*.
33. Debieb, F., & Kenai, S. (2008). The use of coarse and fine crushed bricks as aggregate in concrete. *Construction and Building Materials*, 22, 886-893.
34. Khatib, J.M. (2005). Properties of concrete incorporating fine recycled aggregate. *Cement and Concrete Research*, 35, 763-769.
35. Oikonomou, N.D. (2005). Recycled concrete aggregates. *Cement and Concrete Composites*, 27, 315-318.